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SPECIFICATION

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5 High-temperature solid electrolyte fuel cell comprising a composite of nano-porous thin layer electrodes and a structured electrolyte

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10 The invention relates to a new high-temperature solid electrolyte fuel cell (SOFC) comprising a composite of nano-porous thin layer electrodes and a structured electrolyte. In fuel cells, the chemical energy of a fuel is converted directly into electrical energy with high efficiency and minimal emissions. For this purpose, gaseous fuels (for example hydrogen or natural gas) and air are continually fed into the cell.

The basic principle is realized by the spatial separation of the reactants by an ion conductive electrolyte which, on both sides, is in contact with porous electrodes (anode and cathode). In this way, the chemical reaction between the fuel gas and oxygen is split into two part reactions taking place at the electrode/electrolyte interfaces. The electron transfer between the reactants takes place via an external circuit such that in the ideal case (loss free cell) the free enthalpy of reaction is directly converted into electrical energy. In real cells, the efficiency and power density are coupled by the internal resistance which is largely determined by the polari-

zation resistance of the electrodes. Power density and efficiency can be increased by reducing the internal resistance.

A high-temperature fuel cell usually has an electrolyte of zirconium dioxide ( $\text{ZrO}_2$ ) stabilized with yttrium oxide ( $\text{Y}_2\text{O}_3$ ) (YSZ). At temperatures between 600 and 1000°C and at technically realizable electrolyte densities, this ceramic material shows sufficient conductivity for oxygen ions to achieve an efficient energy conversion.

The electrochemical part reactions take place at the reaction surfaces between the porous electrodes (cathode and anode) and the electrolyte. The main purpose for having porous electrodes is the provision of large reaction surfaces which minimal impairment of gas transport. The larger the reaction surface, referred to as three phase boundary (tpb) between the gas space, electrolyte and electrode, the more current can be transported via the interface at a given polarisation loss. A typical material for the cathode is strontium doped lanthanum manganate ( $(\text{La}, \text{Sr})\text{MnO}_3$ , LSM). A cermet (ceramic metal) of nickel and YSZ serves as anode.

The advantages of high-temperature fuel cells are that, due to the high operating temperatures, various fuels can be reacted directly, that the use of expensive noble metal catalysts becomes redundant and that the operating temperature between 600 and 1000°C makes it possible to use the loss heat as process steam or in coupled gas and steam turbines.

Disadvantages are degradation processes due to the high operating temperature which result in an increase of the internal resistance of the cell.

Such high-temperature fuel cells are the subject of numerous applications for protective rights such as, for example,

DE 43 14 323, EP 0 696 386, WO 94/25994, US 5 629 103,  
DE 198 36 132, WO 00/42621, US 6 007 683, US 5 753 385.

The object of the present invention is to provide a high-  
temperature fuel cell with higher long term stability, higher  
5 current density and lower polarization resistance.

The invention provides a high-temperature solid electrolyte  
fuel cell comprising an electrolyte layer between two elec-  
trode layers obtainable by a process comprising the steps: (i)  
applying electrolyte particles in a screen printing paste onto  
10 an unsintered electrolyte substrate and sintering the struc-  
ture thus produced, (ii) depositing a nano-porous thin elec-  
trode layer by a sol-gel-process or an MOD-process on the  
structure obtained in step (i) and thermal treatment of the  
thus coated structure.

15 This thermal treatment can take place upon immediate putting  
into operation of the fuel cell. The heating up of the fuel  
cell required for this purpose results in a sufficient elec-  
trical conductivity of the structure. The formation of unde-  
sired pyrochlore phases is avoided by this step. Thus, a sepa-  
20 rate sintering process becomes redundant in the production of  
the fuel cell according to the present invention.

The high-temperature solid electrolyte fuel cell according to  
the present invention firstly has an improved interface be-  
tween the electrolyte and electrode layer as compared to fuel  
25 cells described in the prior art. In the fuel cell according  
to the present invention, the effectively usable surface of  
the electrolyte substrate is increased by a structuring in  
order to achieve an increase in the electrochemically active  
three phase boundary. The structured surface is subsequently  
30 coated with a nano-porous thin layer electrode which has a  
layer thickness of 50-500 nm. This layer can be applied by a

sol-gel-process or an MOD (Metal Organic Deposition) process  
(Figure 1).

Optionally, an electrolyte layer can additionally be applied  
on the structured screen printed electrolyte layer by an MOD-  
5 process. This layer can be applied on the cathode and the an-  
ode side of the electrolyte. By means of such an MOD layer,  
consisting of doped zirconium dioxide (yttrium and scandium  
doped) or doped cerium oxide (yttrium, gadolinium or samarium  
doped), negative interactions between electrode and electro-  
10 lyte can be prevented and the start up operation of the cell  
can be shortened or even avoided.

For the preparation of this electrolyte boundary layer, the  
aforementioned components are preferably used in highly pure  
form. The electrolyte boundary layer is preferably very thin  
15 and its preferred thickness is 100 to 500 nm.

The high-temperature solid electrolyte fuel cell according to  
the present invention has the advantage that, due to the in-  
crease of the electrochemically active interface between elec-  
trode and electrolyte by means of structuring the electrolyte  
20 surface, a reduced surface specific resistance, a higher effi-  
ciency at constant surface specific power and a lower electri-  
cal load relative to the electrochemically active interface  
can be achieved. The last mentioned lower electrical load re-  
sults in reduced degradation of the cell and an increase of  
25 the power by a factor of 2 to 3.

With modified cells, power densities of  $1.4 \text{ A/cm}^2$  at a cell  
voltage of 0.7 V and energy densities of  $1.10 \text{ W/cm}^2$  are ob-  
tained (fuel gas:  $\text{H}_2$ , 0.5 l/min, oxidation gas: air, 0.7 l/min,  
electrode surface:  $10 \text{ cm}^2$ ). The cathode performance is strongly  
30 dependent on the microstructure of the interface and the com-  
position of the MOD layer between the electrolyte surface and

the screen printed ULSM layer. Compared to single cells with standard cathodes, an increase of power by 100% at a cell voltage of 0.7 V is achieved by the modification of the cathode (**Figure 2**).

5 During operation for 1,800 h at 950°C, single cells with modified cathodes at 400 mA/cm<sup>2</sup> show a markedly lower voltage degradation (4 mV/1,000 h) than standard cells (35 mV/1,000 h). In long term operation, they have a significantly higher stability than cells with standard cathodes (**Figure 3**).

10 Further advantages of the fuel cells according to the present invention are an increase in the surface specific power at constant efficiency and its cost-efficient production because expensive and chemically pure materials need to be employed only at the electrochemically active regions of the interface.  
15 By the concept of a structured electrolyte surface according to the present invention, an improved adhesion of the electrode layer on the electrolyte is achieved, which, as mentioned above, prevents degradation by delamination.

In the case of an electrolyte supported cell, the structuring  
20 of the electrolyte surface takes place directly upon calendering or, in the case of a cell supported by one of the electrodes or by an electrochemically inactive substrate, by screen printing or spraying.

As electrolyte substrate or supported thin layer electrolyte,  
25 there is preferably used a green sheet or a green (unsintered) electrolyte layer of yttrium doped zirconium oxide (of a suitable solid electrolyte). The screen printing paste is applied thereon.

According to a preferred embodiment of the invention, the  
30 paste has a solid content in the range of 10 to 30%. Higher

solid contents in the screen printing paste result in a reduction of the effective electrolyte surface and, furthermore, in an increase of the average electrolyte thickness. Both result ultimately in a reduction of the electrical performance of an SOFC. For these reasons, the solid content in the screen printing paste must be in the aforementioned range.

Furthermore, it is preferred that the powder fraction of the paste has a particle size distribution in the range of 5 to a maximum of 20  $\mu\text{m}$ .

- 10 The structure on the interface is sintered together with the electrolyte. The advantage therein is that only one sintering step is required and that, due to the higher sintering activity of the powder components in the initial state, an improved adhesion of the structure is achieved.
- 15 The structuring can take place both on the cathode and the anode side. By different doping in the granules or material combinations in the granules (for example different yttrium doping in zirconium dioxide, scandium doped zirconium dioxide (S<sub>z</sub>SZ), gadolinium doped cerium oxide (GCO) etc.) and in the  
20 substrate (yttrium doped zirconium dioxide, doped CeO<sub>2</sub> or scandium doped zirconium dioxide (S<sub>z</sub>SZ) on tetragonal (TZP) zirconium dioxide) lower ohmic losses and an improvement of the material stability are achieved and the use of highly pure costly electrolyte materials can be limited to the interface.
- 25 As mentioned above, the structuring of the electrolyte surface results in an improved adhesion of the electrode. Thus, a delamination of the electrode layer across large areas is prevented (by interlocking the electrode and electrolyte).

Furthermore, the increase of the electrochemically active interface between cathode and electrolyte results in a reduction of the polarization resistance.

Moreover, the granule size of the particles applied as the structuring can be adapted to individual requirements. The structuring can be effected with small or large as well as with small and large granules.

Additional large granules, whose diameter is in the range of the thickness of the electrode layer, improve the support function, reduce the densification of the electrode under the contact bars in the stack because the sintering activity of the electrolyte material is much smaller than that of the cathode and anode materials.

In the production of the fuel cell according to the invention, the deposition of a nano-porous electrode thin layer takes place by a sol-gel-process or MOD-process on the electrolyte surface structured as described above.

For the synthesis of the  $(La_{1-x}Sr_x)M_TO_3$  precursors with  $M_T = Mn, Co$ , the individual propionates of La, Sr, Co and Mn are produced first. These are obtained as solids by reacting  $La_2(CO_3)_3$ , elemental strontium,  $Co(OH)_2$  or  $Mn(CH_3COOH)_2$  with excess propionic acid and in the presence of propionic acid anhydride. By means of these building blocks, it is possible to obtain any desired chemical composition and any desired final stoichiometry of the cathode MOD layer. The individual building blocks can be stored for years. It is also possible to replace or complement some components by other carboxylates, for example acetate, or by diketonates, for example in form of the acetyl acetonates, and thus to provide further building blocks.

For the production of a coating solution with the composition  $\text{La}_{0.75}\text{Sr}_{0.20}\text{MnO}_3$ , the precursors are dissolved in propionic acid in the corresponding stoichiometric ratios. The solid content is typically between 12 and 14 mass % with respect to the oxide. The composition of the coating solutions can be controlled by means of ICP-AES (Inductively Coupled Plasma Atomic Emission Spectroscopy) and the solid content can be controlled thermogravimetrically. The coating solutions can be stored at room temperature for several months. Subsequently, the layers are applied from the liquid phase by spinning (2,000 rpm for 60 sec) or dipping and are stored at 170, 700 and 900°C, respectively, for 15 min. The thickness of a single coating is 80 to 100 nm. Greater thicknesses can be produced by corresponding repetition of the coating procedure **(Figure 4)**.

The nano-porous electrode thin layers deposited by the sol-gel-process or MOD-process described above have the advantage that the nano-porosity throughout the MOD layer enables a high number of three phase boundaries.

As materials for the cathodes there may be used electronic conductor or mixed conductor metal oxides, in particular, perovskites of the composition  $(\text{Ln}_{1-x}\text{A}_x)\text{M}_\text{T}\text{O}_3$  wherein  $\text{A} = \text{Sr}, \text{Ca}$ ,  $\text{M}_\text{T} = \text{Cr}, \text{Mn}, \text{Fe}, \text{Co}, \text{Ni}$ . Examples for such materials are doped  $\text{LaMnO}_3$ , doped  $\text{LaCoO}_3$  and doped  $\text{LaFeO}_3$ .

Material systems for the anode are, for example, Ni, Ni/YSZ, Ni/doped  $\text{CeO}_2$  and doped  $\text{CeO}_2$ .

As mentioned above, the use of such nano-porous MOD electrode thin layers in the fuel cell according to the present invention results in a higher number of three phase boundaries in predominantly electron conducting materials.

Moreover, the stoichiometry and the chemistry of the metal oxides employed, in particular, of the perovskites, can be varied.

Furthermore, due to the low layer thickness and the low process temperatures in the production, it becomes possible to  
5 employ materials which are otherwise chemically and thermomechanically incompatible (for example strontium doped lanthanum cobaltate on YSZ). A further advantage of the nano-porous MOD electrode thin layers is their stability under the operating  
10 conditions of the fuel cell.

The nano-porous MOD electrode thin layers can also be used as intermediate layers. For example, an MOD thin layer electrolyte of 10 mol%  $Y_2O_3$  or  $Sc_2O_3$  doped  $ZrO_2$  (10YSZ/10ScSZ) can be applied to an electrolyte substrate of standard materials (3  
15 or 8 mol%  $Y_2O_3$  doped  $ZrO_2$ ). This thin layer electrolyte, which has higher purity and ionic conductivity, can be produced on the cathode and/or anode side. The MOD electrolyte layer as intermediate layer makes it possible to limit the use of a highly pure but costly electrolyte material to the region of  
20 the electrode/electrolyte interface and thus results in reduced ohmic losses by current constriction as well as to lower polarization resistances due to the formation of secondary phases. The purity requirements of the supporting electrolyte substrate are lowered and the use of cheaper starting materials becomes possible.  
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The invention will be further illustrated by the following examples and the appended figures.

Figure 1 shows a schematic representation of a standard cell (left) and a cell according to the present invention (right)  
30 with modified cathode/electrolyte interface.

Figure 2 shows the current/voltage (I/V) characteristic of single cells with different cathodes at 950°C.

Figure 3 describes the current density as a function of time in the long term operation of a single cell with modified  
5 ULSM-MOD cathode over 1,800 hours at 950°C (degradation rate: 4 mV/1,000 h).

Figure 4 shows an REM image of a nano-porous ULSM-MOD layer on a non-structured 8YSZ electrolyte.

### **Example 1**

10 Single cells with modified ULSM cathodes are produced as follows:

8YSZ particles are applied to 8YSZ green sheets (8YSZ: Tosoh TZ-8Y) by a screen printing process. The particle content in the screen printing paste is selected such that an surface  
15 increase by about 25% is achieved. This structured electrolyte is sintered for one hour at 1,550°C. On the opposite side, a 30-40 µm thick Ni/8YSZ cermet is applied by screen printing as an anode and is sintered for 5 hours at 1,350°C.

Subsequently a single cathode MOD layer of the composition  
20  $\text{La}_{0.75}\text{Sr}_{0.20}\text{MnO}_3$  (ULSM) is applied on the structured side of the electrolyte by spinning and sintered respectively for 15 minutes at 170, 700 and 900°C. The thickness of this layer is about 80 nm. Onto this MOD cathode, a 30-40 µm thick ULSM layer is printed by screen printing.

### **Example 2**

25 Single cells with modified LSC cathodes are produced as follows:

8YSZ particles are applied to 8YSZ green sheets (8YSZ: Tosoh TZ-8Y) by a screen printing process and sintered for one hour at 1,550°C. On the opposite side, a 30-40 µm thick Ni/8YSZ cermet is applied by screen printing as an anode and is sintered for 5 hours at 1,300°C.

Subsequently, a single cathode MOD layer of the composition  $\text{La}_{0.50}\text{Sr}_{0.50}\text{CoO}_3$  (LSC) is applied to the structured side of the electrolyte by spinning and sintered respectively for 15 minutes at 170, 700 and 900°C. The thickness of this layer is about 100 nm. Onto this MOD cathode, a 30-40 µm thick ULSM layer is printed by screen printing.